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TRANSLATOR'S AFFIDAVIT

I, Andrew Wilford, a citizen of the United States of America,  
residing in Dobbs Ferry, New York, depose and state that:

I am familiar with the English and German languages;

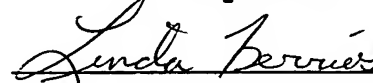
I have read a copy of the German-language document attached  
hereto, namely PCT application PCT/DE03/00599 published 18 Septem-  
ber 2003 as WO 03/076098; and

The hereto-attached English-language text is an accurate  
translation of the above-identified German-language document.

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Sworn to and subscribed before me  
8 September 2004

  
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[TRANSLATION]

DEVICE FOR WITHDRAWING A BAR PRODUCED  
IN A BAR OR PIPE EXTRUDER

The invention relates to a device for withdrawing a bar  
5 produced in a bar or pipe extruder which has at least a driven  
linearly movable carriage which is movable in the withdrawal  
direction of the bar and can exert a tension force upon the bar.

A device of this kind is known from EP 0 300 262 B1. For  
producing a bar of high quality in a bar or tube press [extrusion  
10 press, extruders] it has been recognized as necessary for the bar  
to be withdrawn from the die of the bar or tube press with a  
defined withdrawal force. In this manner it can be ensured that  
the bar formation in the die will not be negatively influenced. To  
ensure a high quality of the bar a withdrawal device has been  
15 described with which the end of the bar to be withdrawn is affixed  
to a carriage movable on a rail. The carriage is connected with  
drive means so that a tension force can be applied to the bar. For  
optimal finishing results, the tension force is a combination of  
different components, whereby especially one component is  
20 determined as a function of the pressed-out bar length.

In this manner the cross sectional tolerances of the bar  
withdrawn from the bar press can be reduced so that the bar has the  
desired quality. This system is based upon the consideration that  
the bar, with increasing spacing from the die, as a result of the

cooling can be loaded with increasing tension without producing a cross sectional change.

It has been found problematical in this context that different forces are applied to the withdrawal carriage over the withdrawal path so that it is very difficult to ensure a defined withdrawal force, for example conforming to a predetermined function, which can be applied to the bar end.

The carriage or puller truck has a mass and is driven by a motor. The speed and torque of the motor can be predetermined by a control. The motor force applied to the carriage, which is converted into the withdrawal force applied to the extrusion pressed profile or strand, will depend upon the friction force of the mounting of the carriage as well as the initial forces which are dependent upon the actual acceleration of the carriage. Only in a static case will the motor force correspond to the withdrawal force, because in that case the speed and the friction are zero. When the profile or strand moves, the friction force and inertial forces on the carriage are not constant and the friction coefficient will depend upon environmental conditions (temperature, contamination of the path). As a consequence it becomes very difficult to apply a defined predetermined withdrawal force to the bar to be withdrawn. If the carriage is accelerated at the beginning of the withdrawal process the force equilibrium is destroyed as a consequence of the inertial forces which arise so that there are special difficulties in maintaining a defined withdrawal force. With light and sensitive profiles or strands

this can give rise to a problem with respect to the quality of the product or to an increase in the waste level in production.

The invention has as its object to improve a device for withdrawing a bar so that the aforementioned drawbacks can be overcome and especially light profiles or strands can be made without loss of quality.

This object is achieved in accordance with the invention in that a second slide or carriage is arranged on the first slide or carriage and which is movable relative to the first slide or carriage in the withdrawal direction, whereby the bar to be withdrawn is engaged with the second carriage.

Through this feature, the entire carriage mass is subdivided into two parts. The first carriage can be moved as has been known. Deviations from a predetermined withdrawal force upon the bar, which can be constant or can vary in accordance with a predetermined function, are compensated by a corresponding dynamic regulation of the second carriage, that is the deviations from the predetermined withdrawal force can be eliminated by the control. Since the second carriage has only a relatively small mass to be moved, the system has a substantially higher dynamic response and enables the predetermined withdrawal force to be maintained with substantially greater precision. The withdrawal force applied to the stand can thus maintain a predetermined profile or pattern or value.

According to a further feature, it is provided that for movement of the second carriage relative to the first carriage, a motor means is used. This motor means is preferably a controllable motor, especially a servomotor.

5                    Preferably the motor means connects the first and second carriages together through transmission means. the transmission means can advantageously be a rack and pinion system, a chain and sprocket system, a cog and cog wheel system or a cable and cable wheel system.

10                   To provide a closed control circuit for the movement of the second carriage, at least one sensor can be arranged on the first and/or second carriage. The sensor should be of the type which is capable of measuring the acceleration of the second carriage (an accelerometer). This should be able to measure  
15 acceleration in a range of precision of  $\pm 1g$ . Furthermore, a sensor can be provided which detects the position of the second carriage relative to the first carriage (displacement meter). Furthermore, a sensor can be provided which detects the force applied by the second carriage to the end of the bar or to the bar  
20 itself (force meter).

The measured signals from the sensor or from the sensors can be fed to the control and/or regulating means which, as a function of the detected measured values by the sensor or the sensors, influences the withdrawal force applied to the bar by the  
25 motor means. Above all it is contemplated here that the control and/or regulating means influence the torque of the motor means.

An exact control of the withdrawal force can be measured when the mass of the first carriage is at least double, preferably at least five times to at least ten times the mass of the second carriage.

5           The device can have more than one first carriage with respective second carriages. The first carriages can then be arranged in cascade one after another in the withdrawal direction.

10           With the proposed configuration, it can be achieved that the withdrawal force which is applied to the bar can be controlled with precision to a predetermined value or in accordance with a predetermined course or pattern, since the system of the invention enables highly dynamic response which permits a precise response to an actual value based upon a predetermined setpoint value.

15           Further details and features of the invention are given in the claims and the description of an embodiment illustrated in the drawing of the invention.

The drawing shows:

FIG. 1 a schematic illustration of a withdrawing device for a bar produced in a bar or tube extrusion press;

20           FIG. 2 the withdrawing device in a three dimensional view;

FIG. 3 a side view of the withdrawing device;

FIG. 4 the withdrawing device of FIG. 3 in plan view;

FIG. 5 the withdrawing device of FIG. 3 in a front view.

In FIG. 1 the conceptional layout of a withdrawing device 1 has been illustrated only highly schematically. In a long known bar or tube extrusion press 2, not shown in greater detail, a bar 3 is extruded which leaves the bar or tube press 2 in a withdrawal direction L. To ensure a high quality bar 3, it is withdrawn by the withdrawal device 1 in the withdrawal direction L with a predetermined withdrawal force.

The withdrawal force can be constant or it can vary along the withdrawal path in accordance with a predetermined function or course (compare EP O 300 262 B1). So that especially also light profiles or strands [extruded bars] can be fabricated with high quality, the withdrawal force which is applied by the withdrawal device 1 to the bar 3 must be maintained with the greatest of precision and for that purpose the withdrawal device 1 has the following construction:

A first slide or carriage 4 is displaceable on a linear guide 11 in the withdrawal direction L to apply the withdrawal force. A motor 12 is provided which can effect the linear movement of the first carriage 4 by a belt 13 and a rerouting roller 14.

On the first carriage 4 there is a linear guide 15 on which a second carriage 5 is disposed so as to be linearly shiftable relative to the first carriage 4 in the withdrawal direction L. The front end 6 of the bar 3 to be withdrawn is connected with the second carriage 5. The second carriage 5 is moved relative to the first carriage 4 by motor means 7 and transmission means 8. The motor means 7 is preferably a

controllable synchronous servomotor. As the transmission means 8, a rack and pinion system has been found to be suitable.

The withdrawal device 1 is equipped with sensors 9 which permit process parameters to be detected. The process parameters being those which may influence the withdrawal force which is applied by the withdrawal device 1 to the front end 6 of the bar 3. In the example, especially an acceleration sensor 9' is provided which detects the acceleration of the second carriage. In addition, a displacement sensor 9" is provided which measures the displacement or relative position of the first side 4 to the second slide 5. A force sensor 9"' detects the withdrawal force applied to the end 6 of the bar 3. The data detected by the sensors 9', 9" and 9"' is applied to a control or regulator means 10. In the latter, especially a setpoint withdrawal force has been stored and is the force which should be applied to the end 6 of the bar 3. This withdrawal force can be variable as a function of the displacement. The control and/or regulating means 10 acts upon the motor means 7 and influences here especially the torque which is produced by the motor means 7.

The first slide or carriage 4 has a mass  $M$  and the mass of the second slide or carriage is designated with  $m$ . To achieve a dynamic response of the control system, the mass of the first carriage 4 should be at least five times and preferably at least ten times the mass  $m$  of the second carriage 5. The mass  $m$  of the second carriage is thus advantageously an order of magnitude smaller than the mass  $M$  of the first carriage 4. A high dynamic



response of the system can be thus ensured first by keeping the movement of inertial of the motor means 7 (servomotor small) Furthermore, the dynamic advantages of the system can be maintained by a stiff construction of the transmission 8, e.g. in the form of a rack and pinion system, thereby positively influencing the dynamic response.

The friction force between the first carriage and the second carriage can be held close to proportional to the speed by a precise machining of the linear guide 15 and shielding it from dirt [contamination]. The friction force can thus be compensated by the computer component of the control and/or regulating means 10.

The inertia of the second carriage 5 is especially low because of the low mass  $m$  of the second carriage so that maintaining the withdrawal force is more easily controllable than with conventional systems.

The first carriage 4 can be driven in known manner with positive control. The friction between the first carriage 4 and its linear guide 11 and the effect of the relatively large mass  $M$  of the first carriage 4 no longer impacts negatively upon the withdrawal force in the bar sensor, since maintaining a predetermined value for the withdrawal force involves corresponding control of the motor means 7 and thus the movement of the second carriage.

In FIG. 2 The withdrawal device 1 has been shown again in a perspective view.

FIGS. 3, 4 and 5 show the withdrawal device in side view plan view and front view. The reference numerals used there correspond to the previously described components or means.

The system can also be configured as a double withdrawal  
5 device which can withdraw one or more strands of the extruded light metal profiles and displace them.

For this purpose, two first carriages are displaceable independently from one another on the liner guide 11 (see FIG. 1 [should be FIG. 4]) so that a handover hand operation or so called  
10 alternating operation, with "flying saw" or a conventional operation with a first carriage 4 is provided. The liner guide can be mounted laterally of the outlet path of the bar 3 on the factory floor.

The double withdrawal device can have respective tracks  
15 [linear guides] for the two carriages whereby a mounting on a truss or support construction laterally of the outlet path of the bar is possible. On the respective second carriages, pneumatically operating profile clamping devices with clamping segments which match the profile contour can be provided to measure a metallic  
20 gripping of the front ends 6 of the bars 3.

The withdrawal device in accordance with the principles explained can be made still finer by providing on the second carriage thus optionally further carriages which like the second carriage can be separately driven.